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Metallographic investigation ...

S/126/61/012/001/015/020
E193/E480

system of intersecting slip lines is formed. Increasing the degree of deformation of molybdenum at 240 to 700°K brings about the appearance of new slip bands and an increase in the displacement along the slip planes. The development of the process of deformation, however, is manifested predominantly by growth of the initially-formed slip bands. Thus, for example, just before the fracture of a specimen ($\delta = 38\%$) at 700°K, the slip bands may become 6 to 7 μ wide. The density of the slip lines also changes with temperature. At 700°K, it is relatively small and slip bands, spaced at 12 to 15 μ , predominate. At 300°K, the density of slip bands corresponding to the same degrees of deformation is higher, the width of the slip bands and the spacing between them decreasing. With a further decrease in temperature, the density of slip bands again decreases approaching that obtaining at 700°K.

(2) In addition to deformation by slip (as revealed by the formation of slip bands) plastic deformation of molybdenum at room temperature entails a specific mode of deformation, localized at the grain boundaries and in the grain-boundary regions. This mechanism operates at relatively low strains (3 to 5%). With increasing strain some of the regions of localized deformation grow

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in size and cracks are formed at the boundaries of these regions after heavy deformation. The width of these near-boundary regions can reach 25 to 30 μ , the relative displacement of adjacent grains along the grain-boundary being several tenths of a μ . This mode of plastic deformation which has been observed in pure iron at sufficiently low temperatures (Ref.4: Gindin I.A. and Starodubov Ya.D. FTT, 1959, 1, 1794) appears to be a property of pure metals. The microstructure and interference pattern of the grain-boundary and the grain-boundary region of molybdenum, deformed at 300°K to $\delta = 20\%$, is shown in Fig.5a and 5b respectively (magnified 440-fold). (3) With decreasing temperature the character of plastic deformation changes considerably. At temperatures approaching the ductile-to-brittle transition, fragmentation and block formation precede the appearance of slip bands. The formation of blocks (whose size, determined with the aid of an electron microscope, was found to be $(2-3) \times 10^{-4}$ cm) increases the resistance of molybdenum to slip and twinning; the process of deformation becomes less uniform and fracture takes place at relatively small strains. (4) In contrast to other metals with

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body-centred cubic crystal structure, twinning plays a relatively insignificant part in the plastic deformation of molybdenum. Thin twins (1 to 2 μ thick) appear in specimens deformed below 246°K but only in isolated grains. An electron microphotograph (magnified 11250 times) of a twin (approx 0.5 μ thick) in molybdenum deformed at 200°K to $\delta = 2\%$ is shown in Fig.8. A specific characteristic of twins of this type is the presence of lightly and heavily distorted zones showing, respectively, as dark and light bands on the microphotograph. It is postulated that the highly distorted zone is formed suddenly when a certain stress, required to initiate the process of twinning, is reached. The appearance of this zone is accompanied by the formation of a mosaic structure in the boundary region and by the formation of blocks and their elastic recovery. As in the case of iron, growth of a twin in molybdenum takes place by movement of one of its boundaries; on reaching the distorted region, the growth of the twin ceases owing to the strain-hardening of this zone. (5) The specific character of plastic deformation of molybdenum is reflected in the manner in which this metal fractures. At 300 and 700°K fracture takes place along the slip planes and a well-defined neck is formed

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in a tensile test piece. Cracks along the slip planes appear also in molybdenum, tested at 240°K, but in this case they are accompanied by cracks along the cleavage planes, the number of these cracks increasing with decreasing temperature. This is illustrated in Fig.9 (magnified 440-fold) showing a portion of a test piece deformed at 243°K to $\delta = 18\%$ in which the parallel slip lines end at a crack along the cleavage plane. On approaching the ductile-to-brittle transition temperature, and particularly below it, cracks along the grain- and block-boundaries are formed. Side by side with the main crack a number of cracks parallel to it but not traversing the entire cross-section of the test piece can be observed. Fracture below the critical temperature is both trans- and inter-crystalline, although the latter is relatively less pronounced. The decrease in strength of molybdenum below 27°K has been attributed to the formation of a large number of surface cracks which cause premature fracture. The formation of the surface cracks is, in turn, associated with a high concentration of oxygen in the surface layer. It was concluded from the results of the present investigation that the character of plastic deformation of 99.95% molybdenum in the temperature interval

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studied changes considerably with decreasing temperature. In the plastic range deformation trans-crystalline slip predominates; at room temperature this mode of deformation is accompanied by localized deformation in the grain-boundary regions. On approaching the ductile-to-brittle transition temperature, block formation plays an increasingly important part and is mainly responsible for the absence of twinning at low temperature. Ductile fracture at 240 to 700°K takes place along the slip planes. At lower temperatures, cohesion of the metal is destroyed in the early stages of the deformation and the main crack develops along the block boundaries. There are 10 figures and 9 references: 5 Soviet and 4 non-Soviet. The four references to English language publications read as follows: Chen N.K., Maddin R. Trans. AIMME, 1951, 191, 461; Andrade E.N., Chow J.S. Proc. Roy. Soc., 1940, 175A, 290; Cahn R.W. J. Inst. Metals, 1954-55, 83, 493; Rendall J.H., Johnstone S.T.M., Carrington W.E. J. Inst. Metals, 1953-54, 82, 345.

ASSOCIATION: Fiziko-tekhnicheskii institut AN UkrSSR
(Physicotechnical Institute AS UkrSSR)

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30456

S/126/61/012/003/016/021

E193/E135

AUTHORS: Garber, R.I., Gindin, I.A., and Shubin, Yu.V.

TITLE: Tensile tests on beryllium single crystals in the
20-500 °C temperature range. V.

PERIODICAL: Fizika metallov i metallovedeniye, vol.12, no.3, 1961,
437-446

TEXT: Scarcity of data on the behaviour of beryllium single crystals under tensile stresses prompted the present authors to undertake the study of this subject. The experimental specimens were prepared from 99.98% pure Be by a pulling-out technique. The orientation of the single crystal tensile test pieces is shown in Fig.1, where p indicates the direction of the applied stress. A strain rate of 0.005%/sec was used in the tensile tests carried out at 20, 200, 400 and 500 °C, helium being employed as the protective atmosphere at elevated temperatures. The mechanical tests were supplemented by metallographic examination. The results of the mechanical tests are reproduced graphically. In Fig.2, the UTS and the yield point (p_b and p_s , kg/mm², left-hand scale)

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Tensile tests on beryllium single ...

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and elongation and reduction of area (δ and ψ , %, right-hand scale) are plotted against the test temperature ($^{\circ}\text{C}$). The fifth curve shows the temperature-dependence of the so-called "diffusion deformation" factor, χ , which is given by $\chi = (1 - \varphi) 100$ $^{\circ}\text{C}$, where φ denotes the deformation localised in the slip on the basal plane, its magnitude being calculated from

$$\varphi = \frac{\sum_i n_i a_{si}}{(\Delta l)_s}$$

where n_i is the number of basal slip bands with the absolute slip displacement of a_{si} , and $(\Delta l)_s = \Delta l \cos 45^{\circ}$ represents the strain of the specimen in the direction of slip. Fig.2 shows the true tensile stress/elongation curve for beryllium single crystals at temperatures indicated by each curve. The effect of temperature on the mode of slip is illustrated in Fig.4, showing (X 200) slip lines on the faces of specimens extended (from left to right) at 20, 200 and 400 $^{\circ}\text{C}$. The variation of the mode of slip with rising temperature was also studied by determining the magnitude of the

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Tensile tests on beryllium single S/126/61/012/003/016/021
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relative slip, γ , and density of the slip bands, ρ , these two parameters being given by $\gamma = b/a_s$ and $\rho = 1/h$ (for the meaning of b/a_s and h see Fig.1). In the regions of uniformly distributed slip lines, γ increased from 0.4 at 20 °C to 2.0 at 500 °C; in the region of macroscopically localised slip, at 400 °C, γ reached 70. The parameter ρ also initially increased with temperature, reaching a maximum of 0.12 $1/\mu$ at 200 °C after which it decreased again, reaching at 400-500 °C a value similar to that at room temperature (~ 0.3 $1/\mu$). Analysis of the results of mechanical tests, correlated with the examination of slip bands and microstructure of specimens after fracture, led to the following conclusions. 1) Plasticity of Be single crystals increases monotonically with rising temperature, showing no peak at 400 °C which is a characteristic of polycrystalline beryllium. The increase in plasticity in the 20-200 °C range is caused by the formation of new slip bands with the material within the bands hardening at a sufficiently fast rate. The increase in plasticity at higher temperatures is associated with the onset of localised slip, characterised by a

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large magnitude of γ (about 70). Both UTS and the so-called strain-hardening modulus \bar{D} passed through a maximum at 200 °C; \bar{D} is given by $\bar{D} = (p_u - p_s)\delta$, where p_u is the true UTS of the metal. This effect is a manifestation of the simultaneously occurring processes of strain-hardening and relaxation.

2) Deformation of Be single crystals with an orientation as illustrated in Fig.1 takes place mainly by slip along the basal planes (0001) in the $[11\bar{2}0]$ direction. At higher temperatures, prismatic slip along the $\{10\bar{1}X\}$ plane in the general $[11\bar{2}0]$ direction and diffusion deformation play an increasingly important part. 3) Brittleness of Be single crystals at room temperature is caused by non-uniform plastic deformation along the basal plane which causes the formation and growth of cracks along the main cleavage plane. At high temperatures, slip becomes more uniform and deformation takes place partly by prismatic slip.

There are 10 figures, 1 table and 1 Soviet-bloc reference.

ASSOCIATION: Fiziko-tekhnicheskiy institut AN USSR
(Physicotechnical Institute, AS Ukr.SSR)

SUBMITTED: January 2, 1961

Card 4/6.

S/126/61/012/006/007/023
E193/E383

AUTHORS: Gindin, I.A., Lazarev, B.G., Starodubov, Ya.D. and
Lazareva, M.B.

TITLE: Mechanical properties of sodium in the range of low-
temperature polymorphic transformations

PERIODICAL: Fizika metallov i metallovedeniye, v. 12, no. 6.
1961, 846 - 852

TEXT: As is the case with Li, the body-centred cubic
crystal structure of Na undergoes a partial change to close-
packed hexagonal on cooling below 35° K. A so-called
"deformation" modification of this metal can be obtained by
straining it plastically at temperatures below 80° K and the
object of the present investigation was to check whether the
effect of low-temperature polymorphism of Na on its mechanical
properties is similar to that observed earlier by the authors
(Ref. 1: FMM, 1960, 10, 472) in Li. To this end, tensile
tests were carried out at 1.6 - 290° K on polished and etched
test pieces of 99.8% pure Na and the following properties were

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E193/E383

Mechanical properties of

determined: 0.2% proof stress; UTS; true tensile strength; elongation; reduction in area and the strain-hardening coefficient. In addition, the microhardness of each fractured specimen was measured at 77 °K, side-by-side with that of a pilot (i.e. untested) specimen. Typical results are reproduced graphically. In Fig. 2, the elongation (b, % - lefthand scale) and reduction in area (ψ , % - righthand scale) are plotted against the test temperature (°K). The temperature-dependence of 0.2% proof stress ($\sigma_{0.2}$), UTS (σ_b) and true tensile strength (σ_u) is reproduced in Fig. 3. Finally, in Fig. 4 the microhardness (H , kg/mm²) measured at 77 °K is plotted against the temperature (°K) to which the test piece had been cooled prior to hardness test; the lower curve relates to pilot specimens, the upper curve representing results obtained near the neck of fractured tensile-test pieces. Several conclusions were reached.

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E193/E383

Mechanical properties of

- 1) Anomalous variation of mechanical properties of Na in the sub-zero temperature range is associated with polymorphic transformations taking place at these temperatures.
- 2) The martensitic transformation which on cooling takes place in Na at about 35 °K is reflected in a sharp increase in its yield strength, UTS and microhardness.
- 3) A minimum in the elongation versus temperature curve is situated in the temperature range within which the deformation-induced polymorphic transformation takes place. The rapid increase in elongation on cooling from 70 to 1.6 °K can be attributed to the deformation-induced change from body-centred cubic to close-packed hexagonal crystal structure.
- 4) The low-temperature polymorphic transformations (particularly the martensitic transformation) bring about an increase in the degree of strain-hardening and uniformity of the plastic flow of Na. There are 4 figures, 1 table and 12 references: 6 Soviet-bloc and 6 non-Soviet-bloc. The four latest English-language references mentioned are:

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Mechanical properties of

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Ref. 2: C.S. Barrett - Phys.Rev., 1947, 72, 245; Acta
crystallog., 1956, 9, 671; Ref. 8: D. Hull, H.M. Rosenberg.
Phys.Rev.Let., 1959, 2, 5; Ref. 10: D. Hull, H.M. Rosenberg -
Phil.Mag., 1959, 4, 303; Ref. 12: D. Guban, J.S. Dugdall,
J. Can. Phys. Rev., 1958, 36, 1248.

ASSOCIATION: Fiziko-tekhnicheskii institut AN UkrSSR
(Physicotechnical Institute of the AS UkrSSR)

SUBMITTED: May 3, 1961

Card 4/0

S/053/61/074/001/001/003
B117/B212

AUTHORS: Garber, R. I., and Gindin, I. A.
TITLE: Physical properties of high-purity metals
PERIODICAL: Uspekhi fizicheskikh nauk, v. 74, no. 1, 1961, 31 - 60

TEXT: The present survey deals with papers which have been published in recent years in the field of high-purity metals. The papers show a trend to obtain specimens of ever-increasing purity. They also show that the progress made varies for different metals (appendix). The physical problems associated with such metals are discussed, for whose analysis the purity of the specimens is decisive. These problems include the electrical resistance, the reflectance of the metals, the magnetic permeability, nuclear reactions, effects of radioactive irradiation, grain boundaries, latent energy of plastic deformation, relaxation, recrystallization, internal friction, moduli of elasticity, and mechanical properties. The latter include the plasticity, deformation curve, cold-brittleness and creeping. A glance at the material available shows that great progress has been made in the analysis of high-purity metals. The most urgent task at present

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Physical properties of ...

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seem to be to develop methods for industrial production of these metals. So far, it has been impossible to solve the problem concerning the changes of physical properties of metal effected by small additions. Regarding the electrical resistance, the joint effect of local distortions by foreign atoms and other causes, such as vacancies etc., may be considered to be proved. The mechanical properties are very sensitive toward additions, especially with respect to structural changes occurring during crystallization or other thermal processes. Vacancies and local distortions seem to play a minor role only. The brittleness of various metals can be eliminated by purifying them from additions. A further development of new methods for the separation of metals will find new fields of application for high-purity metals. References to publications on high-purity metals are given for the following elements: Al, Ba, Be, V, W, Bi, Ga, Ha, Fe, Au, In, Cd, Ka, Ko, Mg, Mn, Cu, Mo, Ni, Nb, Pt, Sn, Pb, Ag, Sr, Sb, Ta, Ti, Th, U, Cr, Zn, and Zr. The following Soviet authors are mentioned: L. S. Kan, B. G. Lazarev (Ref.1: DAN SSSR 81, 1027 (1951); V. B. Zernov, Yu. V. Sharvin (Ref.7: ZhETF 36, 1038 (1959); B. N. Aleksandrov, E. I. Verkin (Ref.8: ZhETF 34, 1655 (1958); A. I. Sudovtsov, Ye. Ye. Semenenko (Ref.18: ZhETF

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Physical properties of ...

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35, 305 (1958); I. M. Lifshits, M. I. Kaganov (Ref.29: UFN 69, 419 (1959); B. Leks (Ref.30: UFN 70, 111 (1960); A. S. Zaymovskiy, G. Ya. Sergeyev, V. V. Titova, B. M. Levitskiy, Yu. N. Sikurskiy (Ref.34: Atomnaya energiya 5, 412 (1958); M. Ya. Gal'perin, Ye. P. Kostyukova, B. M. Rovinskiy, Izv. AN SSSR, ser. tekhn. 4, 82 (1959); D. Ye. Ovsienko, Ye. I. Sosnina, (Ref. 60: Voprosy fiziki metallov i metallovedeniya, sb. no. 9, Kiyev (1959) str. 185); V. A. Pavlov (Ref.64: Fiz. metallov i metallovedeniye 4, 1 (1957); V. A. Zhuravlev, (Ref.72: Zavodskaya laboratoriya 14, 687 (1959); V. S. Yemel'yanov, A. I. Yevstyukhin, D. D. Abonin, V. I. Statsenko, ("Metallurgiya i metallovedeniye chistykh metallov" vyp. 1, 1959, 44). There are 18 figures, 7 tables, and 144 references: 61 Soviet-bloc and 83 non-Soviet-bloc. The six references to English-language publications read as follows: D. J. Maykut, Prod. Engineering 24, 186 (1953) - (Ref.31); A. N. Holden, Phys. Metal. of Uranium Massachus., 1958, str. 7 (Ref.33); J. C. Blade, Rev. metallurgie 54, 769 (1957) (Ref.50); P. Gordon, J. Metals 7, 1043 (1955); (Ref.51); C. Zener, Phys. Rev. 74, 639 (1948) (Ref.68); T. R. Barrett, G. G. Ellis, R. A. Knight, Proc. Sec. Int. Conf. Geneva 2, 319, 320 (1958) (Ref. 100).

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S/181/62/004/002/027/051
B101/B102

AUTHORS: Gindin, I. A., Kozirets, V. V., and Starodubov, Ya. D.

TITLE: Comparison of structural changes in nickel caused by deformation at 4.2 and 300°K and by subsequent creeping

PERIODICAL: Fizika tverdogo tela, v. 4, no. 2, 1962, 465-469

TEXT: Experiments with high-purity nickel (99.994%) tempered at 800°C and 3·10⁻⁶ mm Hg and subsequently deformed by 3.5% at 4.2 or 300°K by stretching are reported. Some of the specimens were subsequently kept at room temperature for 80 - 100 hrs and subjected to creep tests at 700°C and constant pressure (2.8 kg/mm²), while others were heated from 4.2°K to 700°C within 1.5 - 2 min and likewise subjected to creep tests. Both stretching and creeping were carried out with machines described in FMM, 7, 794, 1959. A sharply focused X-ray tube, designed by B. Ya. Pines (Ostrofokusnyye rentgenovskiyе trubki i prikladnoy rentgenostrukturnyy analiz (Sharply Focused X-ray Tubes and Applied X-ray Analysis) GITTL, Card 1/3

Comparison of structural changes in ...

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1955) was used to examine the X-ray structure of the specimens. The disorientation was calculated according to P. B. Hirsch (see below). Results: The original specimens possessed large subgrains (80μ), the lattice was not distorted, and the disorientation was less than 1° .

Disorientation reached 8° at 4.2°K , but was less at 300°K . Specimens deformed at 4.2°K underwent relaxation when heated to room temperature. The distortion of the lattice decreased as a result of polygonization of the subgrain fragments. Microdistortions diminished further on heating to creep temperature. The specimen deformed at 4.2°K and subsequently kept at room temperature had a more uniform and more disperse structure than the specimen heated directly from 4.2°K to 700°C . The removal of microdistortions of the specimens, especially of that deformed at 4.2°K , and the increase in disorientation during the creeping process, indicate that the substructure depends on the temperature at which deformation has taken place. There are 2 figures and 9 references: 8 Soviet and 1 non-Soviet. The reference to the English-language publication reads as follows: P. B. Hirsch, J. N. Kellar, Acta Crystal., 5, 162, 1952.

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Comparison of structural changes in ... S/181/62/004/002/027/05:
B101/B102

ASSOCIATION: Fiziko-tekhnicheskiy institut AN USSR, Khar'kov
(Physicotechnical Institute, AS UkrSSR, Khar'kov)

SUBMITTED: September 22, 1961

GINDIN, I.A.; KOZINETS, V.V.; STARODUBOV, Ya.D.; KHOTKEVICH, V.I.

Structural changes in copper depending on low-temperature deformation and subsequent annealing. Fiz.met.i metalloved. 14 no.6:864-873 D '62. (MIRA 16:2)

1. Fiziko-tekhnicheskii institut AN UkrSSR i Khar'kovskiy gosudarstvennyy universitet.

(Copper--Metallography)
(Metal, Effect of temperature on)

S/032/62/028/001/014/017
B116/B108

AUTHORS: Garber, R. I., Gindin, I. A., Neklyudov, I. M.,
Chechel'nitskiy, G. G., and Stolyarov, V. M.

TITLE: Device for programmed metal hardening

PERIODICAL: Zavodskaya laboratoriya, v. 28, no. 1, 1962, 107 - 109

TEXT: A device has been designed for programming the load on samples. It permits determining the effect of the charging rate on the material properties up to 800°C in a vacuum of 10^{-6} mm Hg or in inert gases. The charging rate can be increased from 10 g/mm² per hr to 3 kg/mm² per hr. Moreover, rates of up to 80 kg/mm² per hr are possible. The maximum load is 350 kg. The sample elongation (up to 4 - 5 mm with an error of 0.5 μ) is measured with an optical strain gauge. Reduction of the charging rate to values corresponding to diffusion hardening lowers both the total deformation and the rate of steady creep. The device (Fig. 1) operates as follows: Dynamometer spring (6) is compressed by the reducing gear (7). The charging rate is regulated by varying the periodic operation of the motor (8) (РД-09 (RD-09)-type) driving the gear

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Device for programmed metal hardening

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(7). The sample is heated by a tubular furnace with molybdenum coil, and the temperature is regulated by an ЭПД-12 (EPD-12) electronic potentiometer. There are 4 figures and 6 Soviet references. ✓

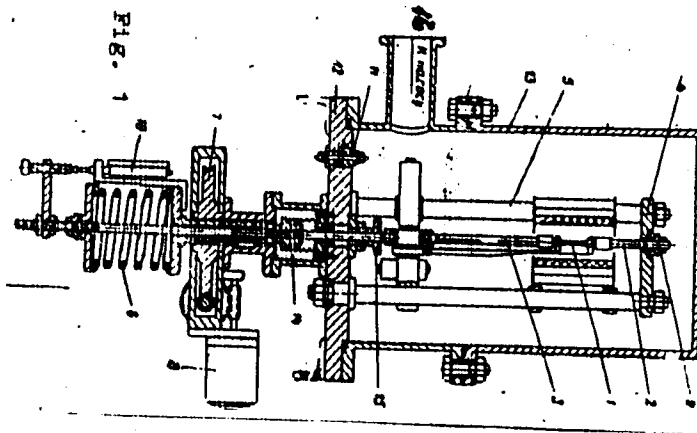
ASSOCIATION: Fiziko-tekhnicheskii institut Akademii nauk USSR (Physico-technical Institute of the Academy of Sciences UkrSSR)

Fig. 1. Diagram of device for programmed hardening.

Legend: (1) sample; (2) and (3) fastenings; (4) cross piece; (5) three bars; (6) dynamometer spring; (7) reducing gear; (8) motor; (9) ball-bearing joint; (10) indicator; (11) mains connection; (12) base plate; (13) vacuum chamber; (14) sylphon; (15) limiter; (16) to pump.

Device for programmed metal hardening

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B116/B108



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GARBER, R.I.; GINDIN, I.A.; MALIK, N.I.; STARODUBOV, Ya.D.

Machine for testing materials for tension and compression at the
temperatures from 1,4 to 1500 K. Zav.lab. 28no.7:865-868 '62
(MIRA 15:6)

1. Fiziko--tekhnicheskii institut AN USSR.
(Testing machines)

37382

S/020/62/143/006/011/024
B164/B101

19.8200

AUTHORS: Gindin, I. A., Starodubov, Ya. D., and Azhazha, V. M.

TITLE: Increase of the creep resistance of nickel by prior deformation at 4.2°K

PERIODICAL: Akademiya nauk SSSR. Doklady, v. 143, no. 6, 1962, 1325-1327

TEXT: The effect of small deformations of nickel at 4.2°K on its creep resistance at higher temperatures was examined by tempering small specimens of high-purity nickel (99.994%) in vacuo at 800°C and then drawing them at 4.2°K, the rate of drawing being 0.03 mm/sec and the degree of deformation 1.7 or 3.5%, afterward establishing the creep curves under a constant stress of 2.8 kg/mm² in vacuo at 700°C. For comparison, tempered specimens which had been deformed at room temperature were used as standards. An increase in creep endurance from 40 to 106 hrs (after 3.5% deformation) and a 4.5-fold increase in creep strength were obtained. Specimens prestrained at 300°C gave much lower values amounting to 51.5 hrs and to a 1.37-fold increase, respectively.

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Increase of the creep resistance, ...

S/020/62/143/006/011/024
B164/B101

Microphotographs of the specimens show that those deformed at 4.2°K present greater homogeneity of fine structure than the others. There are 2 figures and 1 table.

ASSOCIATION: Fiziko-tekhnicheskiy institut Akademii nauk USSR
(Physicotechnical Institute of the Academy of Sciences
UkrSSR)

PRESENTED: January 26, 1962, by G. V. Kurdyumov, Academician

SUBMITTED: September 22, 1961

ACCESSION NR: AT4013981

8/3070/63/000/000/0116/0118

AUTHOR: Gindin, L. A.; Starodubov, Ya. D.

TITLE: Device for metallographic and radiographic investigations of the structure of solid bodies during deformation at low temperatures

SOURCE: Novy*ye mashiny*i pribory*diya ispy*taniya metallov.Sbornik statey. Moscow, Metallurgizdat, 1963, 116-118

TOPIC TAGS: low temperature metallography, low temperature radiography, micro-photography, deformation, metal deformation

ABSTRACT: Devices described in the literature are intended either for determination of mechanical properties of solid bodies at low temperatures, or for low-temperature metallography. However, these devices do not permit direct observation of changes in structure of a specimen during the process of its stressing at low temperatures. Metallographic and usually radiographic investigations of structure of deformed specimens are performed after the specimens have regained room temperature, despite irreversible changes in them. A device has been developed by the authors permitting observation, photographing and taking of motion pictures of changes on the surface of a specimen during cooling, deformation at

ACCESSION NR: AT4013981

low temperature, and subsequent heating. The device is also suitable for radiographic investigations of structure in solid bodies during cooling, low-temperature deformation, and heating. The design of the device permits cooling a specimen down to approximately 10K, measuring this temperature, deforming a specimen in tension or compression, and simultaneously recording values for the "load-deformation" diagram. A schematic illustration of the device is given in Fig. 1 of the Enclosure. The test specimen 1, in the form of flat plate enlarged at its ends, is gripped by jaws 2 located in a depression of the mounting table. One of the jaws is fixed to the table; the other is connected to rod 3 of the loading mechanism and is guided by grooves in the table. The cooling of the specimen to the required temperature is provided through a copper conductor 4 (25 mm in diameter), the lower part of which is immersed in a liquid coolant contained in the vacuum-bottle 5. In order to increase the cooling rate and to reduce the temperature difference between test specimen and coolant, circulation of the coolant is provided through an axial bore in the conductor 4 and tubes 6 and 7. For regulation of the specimen temperature and of the cooling rate, a resistance 8 is provided and a heater 9 in the lower part of the mounting table. The specimen temperature is measured by a thermocouple or a pick-up resistor. The wire connections of the temperature pick-up pass through vacuum insulators 10. The mounting table with the

ACCESSION NR: AT4013981

specimen and part of the cooling conductor are located in a vacuum test chamber 11. The upper part of the chamber is flanged for connection with cover 12. Observation and photographing of the specimen microstructure during the test are conducted through a window in the cover. For observation and photographing of specimen surface changes, the optical part of the device PMT-3 with a photographic attachment are used; and for taking motion pictures, the "Kiyev"-type camera. To avoid condensation of moisture on the specimen, high vacuum is applied to the test chamber 11 by an adsorption-type pump through the hose connection 14. The vacuum is maintained by a thin layer of activated charcoal 15. A copper shield is provided for heat protection of the specimen. The loading device consists of a worm gear reducer 16, driven by the electro-motor 17. The worm gear is mounted on a threaded spindle rotating freely in bushing 18. The bushing is fixed in body 19 of the loading device and takes the thrust during loading of the specimen. The thrust from the spindle is transmitted to a moving cylinder 20, closed from one side and containing the calibrated loading spring 21, acting from one side on the bottom of the cylinder 20 and from the other side on a flange connected to the rod 3 of the movable jaw 2. To a thicker part in the central portion of the rod 3, a bellows 22, having a working stroke of 12 mm, is soldered. The working pins of two dial gages 23 tie to rod 3. The left gage (see Fig. 1 of the Enclosure) is fixed to the body 19 of the device and serves for measuring the absolute elongation (or shortening) of the specimen. The right gage is fastened to the movable cylinder 20 through a plate 24, and

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ACCESSION NR: AT4013981

measures the deflection of spring 21, i. e., the load applied to the specimen. A yoke with three ribs 25 provides greater bending stiffness to conductor 4. The specimen is subjected to a constant-speed axial deformation of 0.03 mm/sec, and a maximum load of 200 kg can be applied. For X-ray investigations at low temperatures, a small chamber for photographing by reflection has been devised (see Fig. 2 of the Enclosure), which can be flanged to the test chamber and sealed by a rubber gasket. A beryllium window 2, 12 mm in diameter and 0.3 mm thick, is used to introduce the X-ray beam into the test chamber. Inside the chamber, a magazine with film 3 is mounted and a sector screen 4 of lead underneath the magazine. The screen permits taking four X-ray pictures without disturbing the vacuum in the chamber, and consequently without heating the specimen. The screen has to be rotated 90° after each exposure. The height of the film magazine location over the sample is adjustable. For making of radiograms, a sharp-focussed X-ray tube designed by B. Ya. Pines is used. A photographic camera can be installed to take microphotographs and radiograms of the same spot of the sample. The residual pressure in the vacuum chamber is 10^{-5} to 10^{-6} mm Hg. The temperature of the specimen depends on the coolant used and is 78K with liquid nitrogen, 25K with liquid hydrogen, and 10K with liquid helium. Orig. art. has: 2 figures.

ASSOCIATION: Fiziko-tehnicheskoy institut AN USSR (Institute of Physics and Technology AN USSR)

Card 4/7

ACCESSION NR: AT4013981

SUBMITTED: 00

DATE ACQ: 20Feb64

ENCL: 02

SUB CODE: MM

NO REF SOV: 010

OTHER: 000

Card 5/7

ACCESSION NR: AT4013981

ENCLOSURE: 01

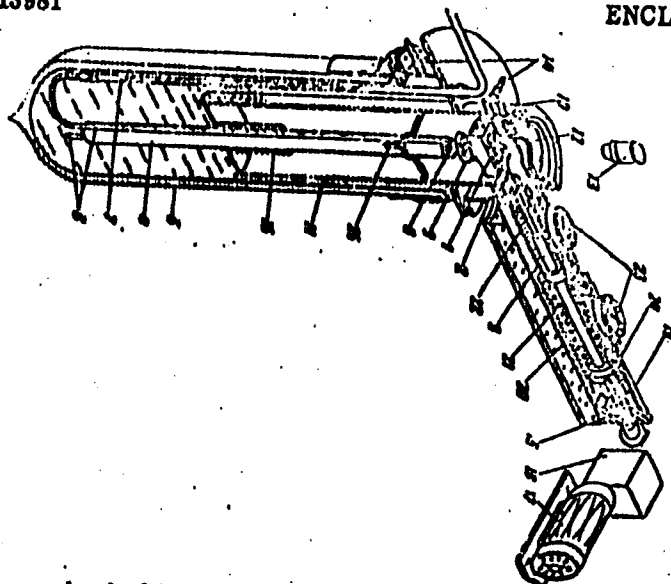


Fig. 1. Device for mechanical tests, metallographic and X-ray investigations at low temperatures

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ACCESSION NR: AT4013981

ENCLOSURE: 02

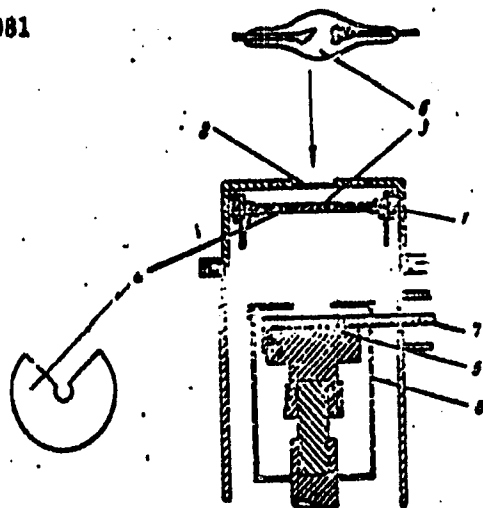


Fig. 2. Chamber for X-ray investigation of structure of solids under deformation at low temperatures. 1 - body of chamber, 2 - beryllium window, 3 - magazine with film, 4 - sector screen (lead), 5 - test specimen, 6 - X-ray tube, 7 - jaw for loading of specimen, 8 - shield

Card

7/7

GARBER, R.I.; GINDIN, I.A.; CHIRKINA, L.A.

Twinning and annealing of nonequilibrium iron-nickel alloy of
the Sikhote-Alin iron meteorite. Meteoritika no. 23:45-55 '63.
(MIRA 16:9)

(Sikhote-Alin Range—Meteorites)

GARBER, R.I.; GINDIN I.A.; SHUBIN, Yu.V.

Compression of beryllium single crystals along the hexagonal axis
in the temperature range 4.2° to 900° K. Fiz. tver. tela 5 no .2:
434-442 F '63. (MIRA 16:5)
(Beryllium crystals) (Strength of materials)

GINDIN, I.A.; KRAVCHENKO, S.F.; STARODUBOV, Ya.D.; GODZHAYEV, V.M.

Apparatus for studying the creep of metals at low temperatures.
Prib. i tekhn. eksp. 8 no.3:169-171 My-Je '63. (MIRA 16:9)

1. Fiziko-takhnicheskii institut AN UkrSSR.
(Creep of metals) (Metals at low temperatures)

GARBER, R.I.; GINDIN, I.A.; STOLYAROV, V.M.; CHECHEL'NITSKIY, G.G.;
CHIRKINA, L.A.

Apparatus for studying the damping of low-frequency torsional
oscillations. Prib. i tekhn. eksp. 8 no.3:172-174 My-Je '63.
(MIRA 16:9)

1. Fiziko-tekhnicheskiy institut AN UkrSSR.
(Oscillations--Electromechanical analogies)

AZHARHA, V.M.; GINBIN, I.A.; STARODUBOV, Ya.D.

Comparing the effect of prestressing at 4.2 and 300° K on the
creep characteristics of nickel at 700°C. Fiz.met. i metallo-
ved. 15 no.1:119-124 Ja '63. (MIRA 16:2)

1. Fiziko-tekhnicheskiy institut AN UkrSSR.
(Nikel—Cold working) (Creep of nickel)

S/126/65/615/005/022/025
E073/E320

AUTHORS: Garber, R.I., Gindin, I.A. and Neklyudov, I.M.

TITLE: Influence of "programmed strengthening" on the creep and recrystallization of iron at elevated temperatures

PERIODICAL: Fizika metallov i metallovedeniye, v. 15, no. 3, 1965, 473-475

TEXT: In earlier investigations on calcite, bismuth and iron, the authors found that in addition to ordinary strengthening caused by lattice distortions during the process of plastic deformation under a continuous load, there is also "programmed strengthening" due to diffusion-blocking and strengthening of weak and overloaded lattice nodes. This produces an increase in the yield point, plasticity at low temperatures and an increased creep resistance. So far, an improvement in the mechanical properties has been observed only at temperatures lower than or equal to the temperature of the programmed treatment. In the work described here, specimens of Fe (0.03% C) were polished and chemically etched, vacuum-annealed at 880 °C for 3 hours and then slowly cooled. After "programmed loading" up to 8 kg/mm at 300 °C at

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S/126/63/015/003/022/025
E073/E320

Influence of

a rate of $90 \text{ g/mm}^2/\text{h}$, the specimens were subjected to a 100-hour creep test at 400°C with a load of 7 kg/mm^2 . The creep rate of previously program-loaded specimens was significantly lower (about $5.6 \times 10^{-3} \text{ \%}/\text{h}$) both in the initial and in the steady-state stages) than that of specimens to which the final load had been applied quickly ($1.3 \times 10^{-3} \text{ \%}/\text{h}$ in the steady-state section). This indicates that overheating does not eliminate the effect of increased resistance to creep of program-strengthened specimens. Microstructures are reproduced of both types of specimens after annealing at 830°C for 5 hours: of specimens loaded at 400°C with a load increasing to 16 kg/mm^2 , whereby the rate of increase varied between 220 and $6 \times 10^{-3} \text{ g/mm}^2/\text{h}$; of specimens loaded quickly. The residual deformations were 1.3 and 1.6%, respectively. The microstructure of specimens which were subjected directly to the final load showed signs of selective recrystallization, whilst the microstructure of the program-loaded specimens was almost the same as prior to annealing. The authors consider the results as a further proof that program-loading leads to a more

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Influence of

S/126/63/015/003/022/025
E073/E320

equilibrated stable structure in that the strengthening does not seem to be accompanied by an increase in the free energy of the crystal. There are 3 figures.

SUBMITTED: August 15, 1962

1. 10109-63

EPF(e)/EPF(z)-2/EPF(q)/VMT(m)/BDS AFFTC/ASD/SSD Pr-1/

Pu-1 WW/JD/IJP(C)

ACCESSION NR: AF3001699

8/0126/63/015/005/0729/0735 14

AUTHOR: Azhazha, V. M.; Gindin, I. A.; Starodubov, Ya. D.; Shapoval, B. I. 11

TITLE: Effect of low-temperature prestrain on the creep and internal friction of copper 18 14

SOURCE: Fizika metallov i metallovedeniye, v. 15, no. 5, 1963, 729-735

TOPIC TAGS: commercial-grade copper, subzero-temperature prestraining, annealing, creep characteristics, internal friction, microstructure changes

ABSTRACT: The effect of low-temperature prestrain on the creep, microstructure, and internal friction of commercial-grade copper was studied. Test specimens annealed in a high vacuum for 2 hr at 850C were prestretched 2.5, 5.0, 7.5, 12.5, or 35% at a constant rate of 0.03 mm/sec at temperatures of 300 or 4.2K. Specimens prestretched at 4.2K were annealed at room temperature for 100 hr. Both groups of specimens were then subjected to short-time creep tests in a vacuum of 0.02 mm Hg at 800C under a stress of 2 kg/mm sup 2. The tests showed that a prestrain of up to 7.5% at room temperature or subzero temperature sharply decreased the rates of the first and second creep stages. The second-stage creep rate, for instance, decreased from 0.95%/hr for annealed specimens, to 0.09 and 0.05%/hr for specimens

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L 10109-63

ACCESSION NR: AP3001689

3

prestrained 7.5% at 300 and 4.2K. The rupture strength of approximately 6.5 hr for annealed specimens increased to approximately 10.0 and 12.3 hr for the specimens prestretched 7.5% at 300 and 4.2K. The purer the metal and the coarser the grain, the higher the effect of prestraining. Oxygen-free copper prestretched 7.5% at 300 or 4.2K and tested under the above conditions had a creep rate of 0.02 or 0.03%/hr and a rupture life of 19.5 or 24 hr. The 10% elongation and reduction of area of the annealed specimen decreased to 4% for the specimens prestrained 7.5% at 4.2 and 300K. Prestrain at 4.2K strengthens grain boundaries and adjacent grain zones and promotes formation of a substructure. This sharply reduces the number of microcracks formed along grain boundaries during creep and inhibits intergranular failure of the metal. Low-temperature prestrain reduces internal friction in copper and significantly increases the temperature at which it begins to rise sharply, e.g., from approximately 100C for annealed specimens to 320 and 470C for specimens prestrained at 300 and 4.2K. Orig. art. has: 1 table and 6 figures.

ASSOCIATION: Fiziko-tekhnicheskiy institut AN USSR (Physicotechnical Institute, AN USSR)

SUBMITTED: 11Nov62

DATE ACQ: 11Jul63

ENCL: 00

SUB CODE: CO
Card 2/274

NO REF SOV: 016

OTHER: 003

E 10751-63
ACCESSION NR: AP3001700
8/0126/63/015/005/0736/0747

AUTHOR: Gindin, I. A., Starodubov, Ya. D.

TITLE: Concerning the ductility of polycrystalline niobium at helium temperatures

SOURCE: Fizika metallov i metallovedeniye, v. 15, no. 5, 1963, 736-747

TOPIC TAGS: mechanical properties of Nb, helium temperatures, microstructure, microhardness, deformation mechanisms, multiple necking, nonductility transition temperature

ABSTRACT: The mechanical properties of Nb in the temperature range from 1.4 to 700K have been investigated. Nb wire (0.1% Ta, 0.028% Ti, 0.05% Fe, 0.05% Si) 3 mm in diameter was drawn to diameters of 1.94, 1.17, or 1.03 mm with process annealing. The specimens were then vacuum annealed at 1800-2400C to remove impurities, especially gases (see Table 1 of Enclosure). The average grain size in all annealed specimens was the same, approximately 75-100 μ . Tensile tests at 1.4-700K at a strain rate of 0.05 mm/sec showed that pure Nb retains substantial ductility even at temperatures close to absolute zero (see Table 2 of Enclosure). Between 200 and 100K the elongation drops; at temperatures below 20K reduction of area rises sharply. At temperatures below 20K the strain-stress curves have a sawlike shape, which is caused by multiple necking. Up to 9 neckings formed on the specimens tested at 4.2K. The microhardness along the gage

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L 10751-63

ACCESSION NR: AF3001700

Length varied from a maximum of 92.5 kg/mm² in the neckings to a minimum of 54-60 kg/mm² between the neckings. Microscopic examination showed that plastic deformation in the whole range from 1.4 to 300K occurs by a slip. Some slip lines were straight and some wavy. Twin crystals were observed only with deformation temperatures and only in some specimens below 77K. "The authors are grateful to B. G. LASSARY for continued interest in the work and for valuable advice." Orig. art. has: 9 figures, 2 tables, and 2 formulas.

ASSOCIATION: none

SUBMITTED: 15Aug62

DATE ACQ: 11Jul63

ENCL: 02

SUB CODE: ML

NO REF SOV: 006

OTHER: 017

Cord 2/K

10049-63 RFP(4)/EVT(4)/BIS ATFTO/ASD JD

ACCESSION NR: AFIC02850

8/0126/63/015/006/0908/0913

AUTHORS: Garbuz, R. I.; Gindin, I. A.; Nakhudov, I. M.

TITLE: Programmed hardening of commercial iron 11

SOURCE: Fizika metallor i metallovedeniya, v. 15, no. 6, 1963, 908-913

TOPIC TAGS: programmed hardening, iron, mechanical property

ABSTRACT: One of the possible methods for improving mechanical properties of solid bodies consists of diffusive blocking and strengthening of weak or over-stressed parts of a specimen. Such parts may develop shearing, sliding surfaces, twinning bands, or dislocation sources. This method was called "the programming of hardening." The device used in the programming procedure is described. It allows the stretching of a specimen at high temperatures and at very small rates of load increase. The commercial iron samples that underwent a programmed hardening at 900C were studied. The tensile test was conducted at the temperature of liquid nitrogen and also at room temperature. The creep test was also conducted at 900C. Preliminary deformation at high temperatures and low rates of loading resulted in: 1) increase of flow limit and hardening modulus; 2) increase in plasticity at the temperature of liquid nitrogen; 3) a substantial decrease in creep velocity;

L 18049-63

ACCESSION NR: AP0002850

3

1) elimination of creeps at 3000. It is concluded that the observed effects are due to a diffusive hardening of weak and overstressed regions in the samples. The authors express their appreciation to Y. M. Stolyarov and G. O. Chechel'nitskiy for their help in the construction of this device. Orig. art. has: 6 figures.

ASSOCIATION: Fiziko-tekhnicheskii institut AN USSR (Institute of Physics and Technology, Academy of Sciences, USSR)

SUBMITTED: 26Jm62

DATE ACQ: 23Jm63

ENCL: 00

SUB CODE: ML

NO REF SOV: 008

OTHER: 001

Card 2/2

GINDIN, I.A.; LAZAREV, B.G.; KHVEDCHUK, I.R.

Dilatometric investigation of the low-temperature deformation
transition to lithium. Fiz. met. i metalloved. 16 no. 5: 793-794
N '63. (MIRA 17:2)

1. Fiziko-tehnicheskii institut AN UkrSSR.

ACCESSION NR: AF4037066

S/0129/64/000/005/0044/0046

AUTHOR: Gindin, I. A.; Lazareva, M. B.; Nikishov, A. S.; Rink, L. P.; Starodubov, Ya. D.; Yarov, I. A.

TITLE: Mechanical properties of structural alloys at low temperature

SOURCE: Metallovedeniye i termicheskaya obrabotka metallov, no. 5, 1964, 44-46

TOPIC TAGS: alloy, structural alloy, austenitic iron alloy, Kh25N16G7AR alloy, Kh12N20T3R alloy, Kh16G9AN4 alloy, KhN35VTYu alloy, titanium alloy, OT4 alloy, copper alloy, BrKh08 alloy, ZhS6KP alloy, steel, martensitic steel, VNS2 steel, EI659 steel, cryogenic alloy

ABSTRACT: Mechanical properties and fracture tests of Kh25N16G7AR, Kh12N20T3R, Kh17G9AN4, KhN35VTYu; austenitic iron base alloys VNS2 (EP225) and EI659, martensitic steels, ZhS6KP high-strength alloy, OT4 titanium alloy, BGKh08 copper alloy, and other [unidentified] alloys were investigated at temperatures in the 4.2—300K range.

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ACCESSION NR: AP4037066

Specimens (either flat with a cross section of 1.5 x 2 mm or round and 2.2 mm in diameter) were tested in a heat-treated condition [shown in the article]. With a decreasing test temperature the resistance to plastic deformation and the tensile strength of all alloys increased. This was found to be particularly pronounced in the case of VNS2 alloy which at 293, 77, and 20K had a tensile strength of 97.5, 155.0, and 180.0 kg/mm² (annealed at 950C, air cooled, and tempered at 620C for 1 hr). All alloys were found to maintain some ductility at temperatures as low as that of liquid hydrogen except for E1659 steel and OT4 alloy which failed with respective elongations of 0% (at 20K) and 0.7% (at 77K). The elongation of the VNS2 alloy, on the contrary, was found to increase with a decrease of temperature from 15% at 293K to 20% at 20K. BGKh08 copper-base alloy was also very ductile at low temperatures (at 4.2K an elongation of 18.6%). A simultaneous increase of the ductility and strength of VNS2 alloy might be explained by some changes of phase composition under the effect of low-temperature deformation. All the materials tested at temperatures down to 20K yielded uniformly, some with, some without necking. Only in the case of the VNS2 steel did the strain-stress curve at 20K have a saw-like

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ACCESSION NR: AP4037066

shape. However, at temperatures above 20K the steel yielded uniformly. The fracture mode was ductile with clearly expressed necking even at 20K. Orig. art. has: 1 figure and 1 table.

ASSOCIATION: Fiziko-tekhnicheskii Institut AN USSR (Physico-technical Institute, AN USSR)

SUBMITTED: 00

DATE ACQ: 05Jun64

ENCL: 00

SUB CODE: MM

NO REF SOV: 002

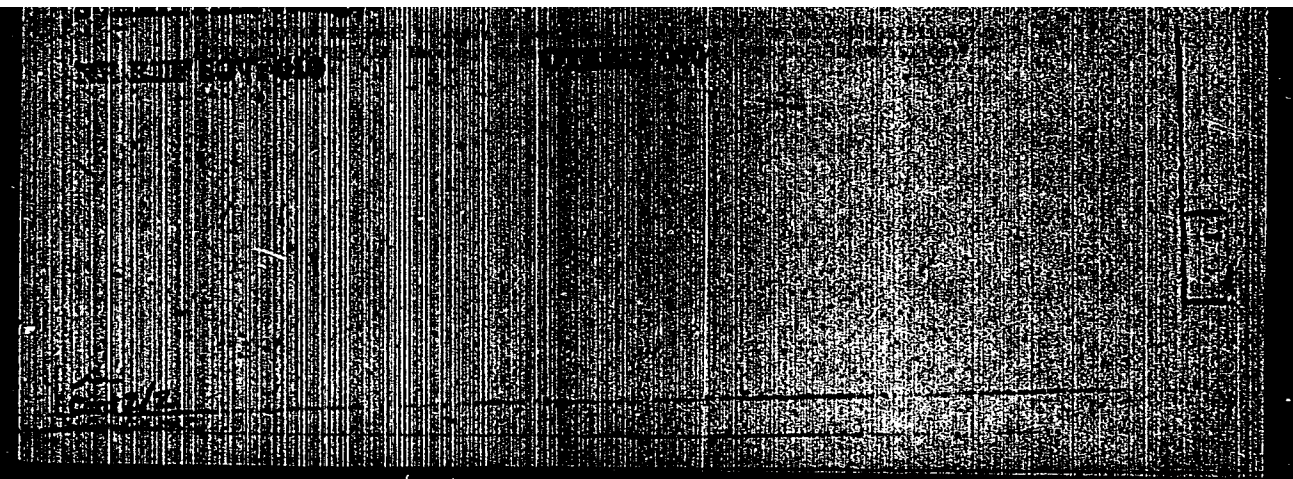
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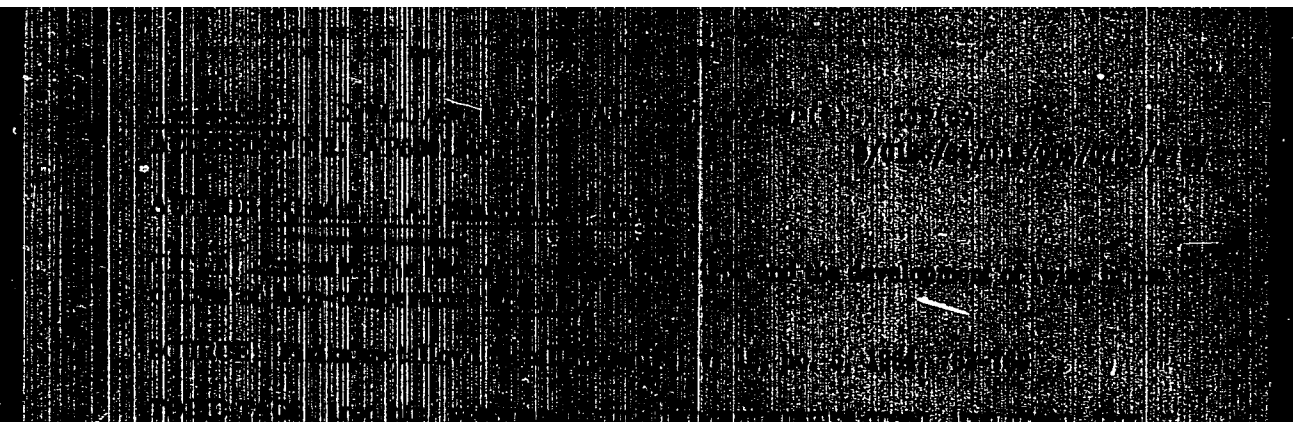
GARBER, R.I.; GINDIN, I.A.; MOGIL'NIKOVA, T.T.; NEKLINOV, I.M.

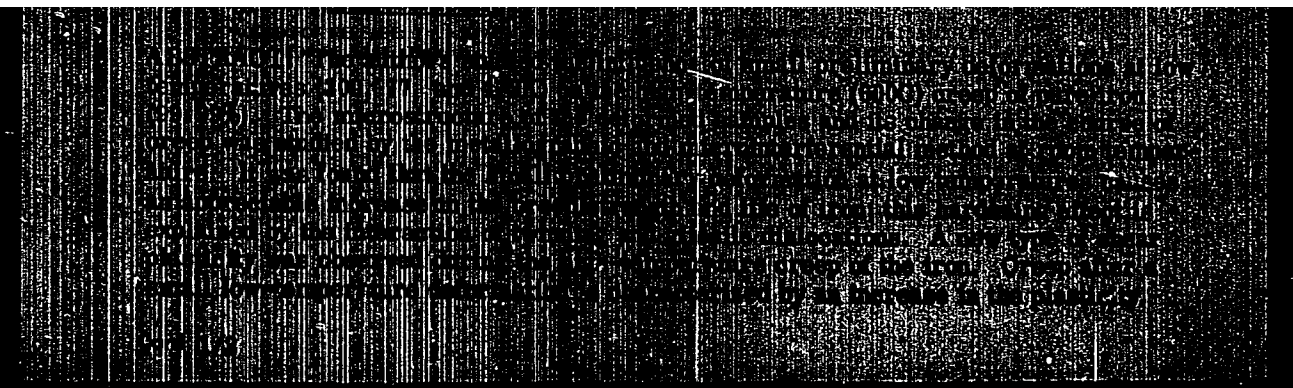
Internal friction of iron hardened by programming. Fiz. met. i
metalloved. 18 no.3:443-447 S '64. (MIRA 17:11)

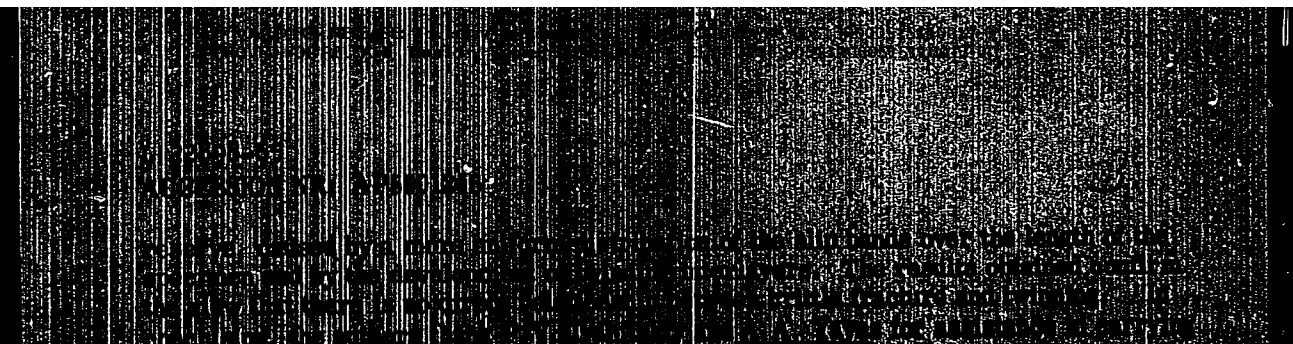
1. Fiziko-tekhnicheskii institut AN UkrSSR.

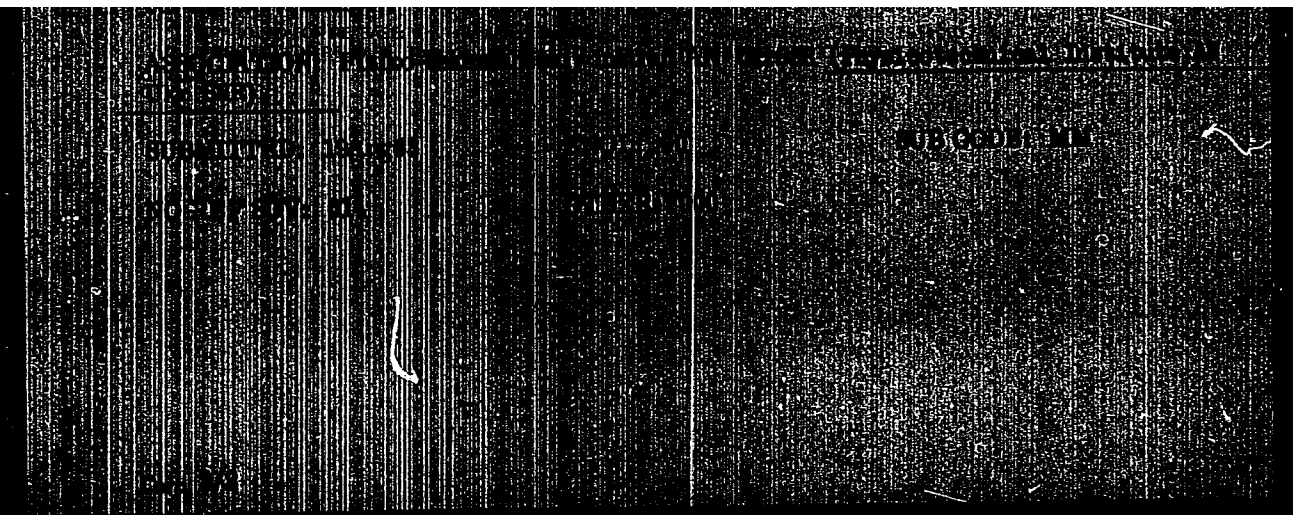












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GINDIN, I.A.; KERLYUDOV, I.M.; SMELOVA, D.F.

Influence of grain size on the effect of iron hardening during
programmed loading. Fiz. met. i metalloved. 19 no.4:627-629
kp 1966. (MIRA 18:66)

2. Fiziko-tekhnicheskiy institut AN UkrSSR.

I.8841-66 EWP(m)/T/EWP(t)/EWP(b)/EWA(c) IJP(c) JD/JG

ACC NR. AP5027148

UR/0126/65/020/004/0603/0607

AUTHOR: Garber, R.I., Gindin, I.A.; Chirkina, L.A.

ORG: Physicotechnical Institute, AN UkrSSR (Fiziko-tekhnicheskii institut AN UkrSSR)

TITLE: Low temperature "deformation" polymorphism in lithium by the internal friction method

SOURCE: Fizika metallov i metallovedeniye, v.20, no.4, 1965, 603-607

TOPIC TAGS: lithium, phase transition, internal friction

ABSTRACT: Measurements were made by the method of damping free torsional vibrations of the samples in the temperature interval embracing the transition from a body-centered cubic lattice to a face-centered cubic lattice (78-200°K), at frequencies of 0.7, 0.8 and 1.3 cycles, in the region independent of amplitude. The logarithmic decrement of damping was taken as the measure of internal friction. The lithium samples, of a purity of 99.3%, were prepared by pressing in the mold at room temperature under a layer of kerosene for protection from oxidation. The length of the effective cylindrical section of each sample was 30 mm and the diameter 3 mm. For stress measurements, the sample was annealed for 2-3 days at 300°K, then pickled in methyl alcohol and

Card 1/2

UDO: 548.33:539.67

L 0011-06

APPROVED FOR RELEASE: Thursday, September 26, 2002

CIA-RDP86-00513R000515110017-0

ACC NR 215027748

APPROVED FOR RELEASE: Thursday, September 26, 2002

CIA-RDP86-00513R000515110017-0

cooled to the temperature of liquid nitrogen (78°K), at which temperature it does not oxidize or undergo phase transition, and was mounted in the apparatus for measurement of internal friction in the single phase state (body-centered cubic). To induce the polymorphic transition from the body-centered cubic to the face-centered cubic lattice and to investigate internal friction, part of the samples were previously deformed by torsion at 78°K up to the relative shear, 5.2×10^{-2} . The martensite nature of the "deformation" nature of the transition from a body-centered to a face-centered cubic lattice in lithium is marked in an especially clear manner in experiments on measurement of internal friction during heating of the samples to determined temperatures above and below the temperature of the reverse transitions with intermediate cooling to 78°K, as well as in a study of the frequency dependence of internal friction. Orig. art. has: 3 figures.

SUB CODE: MM, 10/ SUBM DATE: 28Oct64/

ORIG REF: 010

OTH REF: 005

SVK

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2/2

L 24575-66 INT(m)/T/INF(t) IJP(s) JD/JH

ACC NR: AP6009671

SOURCE CODE: UR/0181/66/008/003/0842/0845

AUTHORS: Bezuglyy, P. A.; Gindin, I. A.; Neklyudov, I. M.;
Rabukhin, V. E.

58
6

ORG: Physicotechnical Institute of Low Temperatures AN UkrSSR,
Khar'kov (Fiziko-tekhnicheskii institut nizkikh temperatur AN UkrSSR)

TITLE: Securing of dislocations on point defects during programmed
loading of aluminum single crystals

SOURCE: Fizika tverdogo tela, v. 8, no. 3, 1966, 842-845

TOPIC TAGS: hardening, crystal dislocation phenomenon, crystal
defect, static load test, ultrasonic absorption, aluminum, single
crystal

ABSTRACT: This is a continuation of earlier work (FMM v. 18, 443,
1964 and earlier papers) dealing with various hardening mechanisms
that can be activated by varying the rate of increasing an external
stress on a crystal and the possibility of programming the hardening
on the basis of such mechanisms. The present paper presents the re-

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L 24575-66

AGC NR: AP6009671

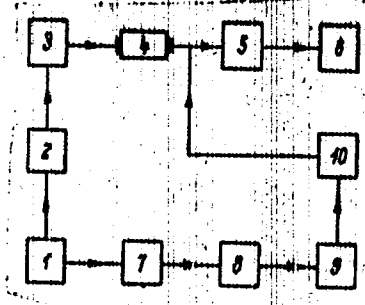


Fig. 1. Block diagram of pulsed ultrasonic installation. 1 -- Master pulse generator, 2 -- modulator, 3 -- high frequency generator, 4 -- sample, 5 -- superheterodyne receiver, 6 -- oscilloscope, 7 -- controlled pulse delay, 8 -- pulse generator, 9 -- standard hf generator, 10 -- attenuator.

sults of an investigation of the dependence of absorption of longitudinal ultrasound on the level of prestressing attained during programmed (slow) hardening of single-crystal aluminum, and the results obtained with fast loading are also given for comparison. Both annealed and non-annealed samples were tested. The absorption was measured by comparing two successive reflected pulses, using an ultrasonic pulsed setup (Fig. 1). All measurements were made with a longitudinal compression-rarefaction wave operating at 72 Mc. From

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2/3

L 24575-66

ACC NR: AP6009671

the obtained plots of the ultrasound absorption against the loading it is concluded that securing of dislocations during the earlier stages of the programmed loading is possible. At large degrees of deformation, a maximum of ultrasound absorption is observed. The results are interpreted from the point of view of the dislocation theory of absorption developed by A. Granat and K. Lucke (J. Appl. Phys. v. 28, 583, 1956). Orig. art. has: 3 figures, 5 formulas, and 1 table. 0

SUB CODE: 20/ SUBM DATE: 28Jul65/ ORIG REF: 006/ OTH REF: 001

Card

3/3 BK

ACC NR: AP6017510 (N)

SOURCE CODE: UR/0126/66/021/035/0774/0778

AUTHORS: Gindin, I. A.; Neklyudov, I. M.; Pinkel', V. A.; Shubin, Yu. V.

ORG: Physico-technical Institute, AN UkrSSR (Fiziko-tehnicheskii institute AN UkrSSR)

TITLE: Effects of programmed loading on the plasticity of beryllium monocrystals

SOURCE: Fizika metallov i metallovedeniye, v. 21, no. 5, 1966, 774-778

TOPIC TAGS: beryllium, metal property, metal crystal, crystal property, plasticity

ABSTRACT: The effects of preliminary programmed loading at 400C on the subsequent mechanical properties of beryllium monocrystals at room temperature were investigated. One set of specimens (99.6% pure, with base plane oriented at 45° to the loading axis) was loaded (0, 5, 6, and 10 kg/mm²) and tested in compression. Another set (99.9% pure, base plane and <1010> direction coincided with loading axis) was loaded (0, 4.3, and 5 kg/mm²) and tested in tension. It was found that the room temperature yield stress σ_s and relative compressibility ϵ were 9.6, 11.3, 11.0, and 9.8 kg/mm² and 10.7, 17.7, 24.7 and 11.2% respectively for the preloading conditions of the first set of specimens and 14.5, 16.1, and 12.4 kg/mm² and 29, 36, and 39.5% respectively for the second set. Elongation was 54, 53, and 64% respectively for the second set. X-ray diagrams of the preloaded monocrystals are also presented. Orig. art. has: 5 figures.

SUB CODE: 11, 13/ SUBM DATE: 31May65/ ORIG REF: 006/ OTH REF: 006

Card 1/1/2/2/2

UDC: 539.37:546.45

ACC NR: AP6033052

SOURCE CODE: UR/0126/66/022/002/0254/0261

AUTHOR: Gindin, I. A.; Starodubov, Ya. D.; Zakharov, V. I. 43

ORG: Physicotechnical Institute, AN UkrSSR (Fiziko-tekhnicheskii institut AN UkrSSR) B

TITLE: Investigation of the effect of low-temperature deformation on the creep resistance of nickel and copper at high temperatures 17 41

SOURCE: Fizika i metallov i metallovedeniye, v. 22, no. 2, 1966, 254-261

TOPIC TAGS: nickel, creep, ~~resistance~~, copper, ~~creep resistance~~, ~~nickel~~ ~~mechanothermal treatment~~, ~~copper~~ ~~mechanothermal treatment~~ mechanical heat treatment, rupture strength

ABSTRACT: Specimens of oxygen-free copper (99.98%-pure) and vacuum-melted nickel (99.95%-pure), vacuum-annealed at 1050C (nickel) and 900C (copper) for 4 hr, were subjected to low temperature mechanothermal treatment (LMTT) stretched by 3.7% (nickel) or 8% (copper) at 4.2 and 300K, and "annealed" at room temperature for about 100 hr. The specimens were then tested for creep resistance at temperatures ranging from 500C to 1000C. It was found that LMTT improved considerably the rupture life of both metals. For instance (see Fig. 1), the rupture life of untreated nickel specimens at 800C under a stress of 1.3 kg/mm²

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UDC: 548.0:539

L 08716-66

APPROVED FOR RELEASE: Thursday, September 26, 2002

CIA-RDP86-00513R000515110017-0
CIA-RDP86-00513R000515110017-0

ACC NR: AP6033052

Elongation

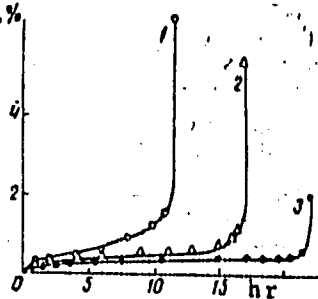


Fig. 1. Primary creep curves of nickel at 800C under a stress of 1.3 kg/mm²

1 - Untreated specimen; 2 and 3 - specimens stretched at 300 and 4.2K, respectively.

was 11.3 hr, the elongation was 6.5%; the rupture life of specimens deformed at 300 and 4.2K was 17 and 22 hr, and the elongation was 5.8 and 2.0%, respectively. The creep resistance of copper specimens was similarly affected by LMTT. The effect of LMTT on creep behavior is preserved at temperatures up to 1000C for nickel and up to 700—750C for copper. Orig. art. has: 3 figures and 3 tables.

SUB CODE: 13, 11/ SUBM DATE: 10Aug65/ ORIG REF: 011/ OTH REF: 001

ACC NR: AP7004567 SOURCE CODE: OR/0126/66/021/004/0600/0607

AUTHOR: Girdin, I. A.; Godzhayev, V. M.; Lazareva, M. B.; Starodubov, Ya. D.

ORG: Physicotechnical Institute, AN UkrSSR (Fiziko-tokhnichosky institut AN UkrSSR)

TITLE: Low-temperature creep of lithium in the region of polymorphous transformation

SOURCE: Fizika metallov i metallovodeniye, v. 21, no. 4, 1966, 600-607

TOPIC TAGS: creep, metal deformation

ABSTRACT: A study was made of creep in Li at 300, 180 and 77 K., encompassing the polymorphous transformation range. The electrical resistance of specimens during the creep process was measured. It is shown that for long-term low-temperature creep of Li, the creep curves show three stages, instantaneous deformation, a transitional stage and a stage of steady flow. At 77 K. the logarithmic rule of the transitional stage of creep is valid up to those values of stress at which polymorphous transition is absent or weakly defined. Creep curves of single-phase specimens at 300 K. even in the case of low stresses, do not comply with the logarithmic rule. A maximum of electrical resistance during creep at 77 K. was found which decreases in a steady pattern in specimens previously strained at 77 K. Orig. art. has: 8 figures.

[JPRS: 36,774]

SUB CODE: 20 / SUBM DATE: 09Mar65 / ORIG REF: 005 / OTH REF: 009

ACC NR: AP6022042

(A)
SOURCE CODE: UR/0120/66/000/003/0225/0226

AUTHOR: Gindin, I. A.; Starodubov, Ya. D.; Kravchenko, S. F.; Lazareva, M. B.

ORG: Physico-Technical Institute, AN UkrSSR, Khar'kov (Fiziko-tehnicheskii institut AN UkrSSR)

TITLE: A device for rolling metals at temperatures of 4.2-300°K

SOURCE: Priory i tekhnika eksperimenta, no. 3, 1966, 225-226

TOPIC TAGS: low temperature physics, low temperature metal, low temperature research, metal rolling

ABSTRACT: The device is used to measure the electrical resistance of deformed samples and for carrying out heat treatment in the temperature range from 4.2 to 1000°K. The basic characteristics of the setup are as follows: roller diameter--30 mm; operating length of the rollers--20 mm; rolling speed--1 and 10 mm/min; initial cross section of samples--from 3 to 5 mm² (depending on the material). The thickness of the foil obtained is on the order of ten microns. For example, for copper at 20°K, the thickness is 20-30 microns. Orig. art. has: 1 figure.

SUB CODE: 11,20,13/

SUBM DATE: 24Apr65/

ORIG REF: 002/

OTH REF: 002

UDC: 621.59:621.771

Card 1/1

ACC NR: AP7001543

SOURCE CODE: UR/0020/66/171/003/0552/0554

AUTHOR: Gindin, I. A.; Starodubov, Ya. D.; Lazareva, M. B.; Lazarev, B. G.
(Academician AN UkrSSR)

ORG: Physicotechnical Institute Academy of Sciences UkrSSR (Fiziko-tehnicheskii
institut Akademii Nauk UkrSSR)

TITLE: Low-temperature recrystallization of copper rolled at 77 and 20K

SOURCE: AN SSSR. Doklady, v. 171, no. 3, 1966, 552-554

TOPIC TAGS: copper, low temperature deformation, ~~copper~~^{metal} deformation, ~~copper~~^{metal} metal
recrystallization, recrystallization temperature, recrystallization activation energy,
~~metal rolling~~^{grain size, metal physical property}

ABSTRACT: Specimens of 99.98%-pure copper with an initial grain size of 100 μ were
rolled at 293, 77, and 20K with a 10% reduction per pass and a total reduction
of 90%. The specimens were rolled at a speed of 10 mm/min and immediately annealed
at 293-468K. X-ray diffraction pattern examination showed that low-temperature
deformation decreased the grain size, produced noticeable microdistortion in the
lattice, and significantly reduced the temperature of the beginning of recrystalliza-
tion. Copper deformed with a 90% reduction recrystallized even at room temperature.
The lower the deformation temperature, the sooner the recrystallization begins.
For instance, in copper rolled at 20K the recrystallization begins after 19 hr,
while in copper rolled at 77K-after 2.5 month. With decreasing deformation tempera-

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UDC: 539.2

ACC NR: AP7001543

ture from 293 to 20K, the activation energy was found to decrease from 33 to 18 kcal/g-atom. This fact, and also the lowering of the recrystallization temperature, is caused by an increase in the latent deformation energy and by a higher metastability of the crystalline body. The low-temperature recrystallization makes it possible to investigate the metal recrystallization, taking into account the temperature conditions of the activation work straining, and to develop metal structures with special physical properties. V. V. Kozinets and M. P. Starolat are thanked for their assistance in the experiments. Orig. art. has: 2 figures.

SUB CODE:11,24/13/SUBM DATE: 15Jul66/ ORIG REF: 008

ACC NR: AF7009206

SOURCE CODE: UR/0185/66/011/011/1243/1246

AUTHOR: Hindin, Y. A.--~~Gindin, I. A.~~; Malik, H. M.--Malik, G. N.; Nechvolod, M. K.--
Nechvolod, N. K; Starodubov, Ya. D.

ORG: Physicotechnical Institute AN UkrSSR (Fiziko-tekhnicheskiy institut AN UkrSSR);
Pedagogical Institute, Khar'kov (Pedagogicheskiy institut)

TITLE: Effect of ultrasonic irradiation on the creep of LiF single crystals, II.

SOURCE: Ukrayins'kyi fizychnyy zhurnal, v. 11, no. 11, 1966, 1243-1246

TOPIC TAGS: lithium fluoride, creep, ultrasonic irradiation, crystal dislocation
phenomenon, plastic deformation, crystal defect

ABSTRACT: Part I is published in the same issue as part II, which reports an investi-
gation of the influence of prior low-intensity ultrasonic irradiation on the creep of
single crystals of LiF to which the load was applied in steps, and the influence on
the change in the dislocation structure. The investigations were made on single
crystals measuring $1.5 \times 2 \times 5$ mm having a dislocation density $6 \times 10^4 - 1 \times 10^5$
 cm^{-2} . The method of preparing the samples and their etching are described in part I.
The creep tests were made under uniaxial compression and under identical conditions.
The results show that prior irradiation weakens the samples, leading to an increase
in the plastic deformation and to an increase in the creep rate. Prior ultrasonic
irradiation also contributes to the lowering of the stress required for the transi-
tion from the deformation damping stage to the stage where the deformation increases

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ACC NR: AF7005206

rapidly under stepwise creep conditions. The results are interpreted from the point of view that the ultrasound lowers the potential barrier for the motion of the dislocations in the crystal and facilitates their motion. It is also possible that point defects are produced under the influence of the ultrasound. Orig. art. has: 5 figures.

SUB CODE: 20, 11/ SUBM DATE: 31Jan66/ ORIG REF: 004/ OTH REF: 008

KUPERMAN, Yakov Mironovich, kand.ekon.nauk; YAKUSHEV, Pavel Mikhaylovich. Prinimal uchastiye: GINDIN, I.P., kand.ekon.nauk;
BIRMAN, A.M., kand.ekon.nauk, red.; KUTSENOVA, A.A., red.isd-va;
ML'KINA, E.M., tekhn.red.; GILENSON, P.G., tekhn.red.

[Working capital of construction organizations] Oborotnye
sredstva stroitel'nykh organizatsii. Moskva, Gos.izd-vo lit-ry
po stroit., arkhitekt. i stroit.materialam, 1959. 159 p.

(MIRA 12:8)

(Construction industry--Finance)

GINDLIN, I.M., inzh.

New cold storage distribution warehouses of the Kazakhstan S.S.R.
Khol.tekh. 40 no.5:4-7 S-0 '63. (MIRA 16:11)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut kholodil'noy
promyshlennosti.

GINDIN, I.S., tekhnik-tekhnolog; ANDREYEV, V.M., prof., otv.red.;
POSTERNYAK, Ye.F., inzh., red.; FREGER, D.P., tekhn.red.

[Swivel carriage for cutting screw threads on turret lathes]
Povorotnyi support dlia narezaniia rez'by na revol'vernykh
stankakh. Leningrad, 1954. 5 p. (Informatsionno-tekhnicheskii
listok, no.6(579)). (MIRA 14:6)

1. Leningradskiy Dom nauchno-tekhnicheskoy propagandy. 2. Lenin-
gradskiy Dom nauchno-tekhnicheskoy propagandy (for Posternyak).
(Lathes---Attachments)

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1992, 1993, 1994, 1995, 1996, 1997, 1998, 1999, 2000, 2001, 2002, 2003, 2004, 2005, 2006, 2007, 2008, 2009, 2010, 2011, 2012, 2013, 2014, 2015, 2016, 2017, 2018, 2019, 2020, 2021, 2022, 2023, 2024, 2025, 2026, 2027, 2028, 2029, 2030, 2031, 2032, 2033, 2034, 2035, 2036, 2037, 2038, 2039, 2040, 2041, 2042, 2043, 2044, 2045, 2046, 2047, 2048, 2049, 2050, 2051, 2052, 2053, 2054, 2055, 2056, 2057, 2058, 2059, 2060, 2061, 2062, 2063, 2064, 2065, 2066, 2067, 2068, 2069, 2070, 2071, 2072, 2073, 2074, 2075, 2076, 2077, 2078, 2079, 2080, 2081, 2082, 2083, 2084, 2085, 2086, 2087, 2088, 2089, 2090, 2091, 2092, 2093, 2094, 2095, 2096, 2097, 2098, 2099, 2100, 2101, 2102, 2103, 2104, 2105, 2106, 2107, 2108, 2109, 2110, 2111, 2112, 2113, 2114, 2115, 2116, 2117, 2118, 2119, 2120, 2121, 2122, 2123, 2124, 2125, 2126, 2127, 2128, 2129, 2130, 2131, 2132, 2133, 2134, 2135, 2136, 2137, 2138, 2139, 2140, 2141, 2142, 2143, 2144, 2145, 2146, 2147, 2148, 2149, 2150, 2151, 2152, 2153, 2154, 2155, 2156, 2157, 2158, 2159, 2160, 2161, 2162, 2163, 2164, 2165, 2166, 2167, 2168, 2169, 2170, 2171, 2172, 2173, 2174, 2175, 2176, 2177, 2178, 2179, 2180, 2181, 2182, 2183, 2184, 2185, 2186, 2187, 2188, 2189, 2190, 2191, 2192, 2193, 2194, 2195, 2196, 2197, 2198, 2199, 2200, 2201, 2202, 2203, 2204, 2205, 2206, 2207, 2208, 2209, 2210, 2211, 2212, 2213, 2214, 2215, 2216, 2217, 2218, 2219, 2220, 2221, 2222, 2223, 2224, 2225, 2226, 2227, 2228, 2229, 2230, 2231, 2232, 2233, 2234, 2235, 2236, 2237, 2238, 2239, 2240, 2241, 2242, 2243, 2244, 2245, 2246, 2247, 2248, 2249, 2250, 2251, 2252, 2253, 2254, 2255, 2256, 2257, 2258, 2259, 2260, 2261, 2262, 2263, 2264, 2265, 2266, 2267, 2268, 2269, 2270, 2271, 2272, 2273, 2274, 2275, 2276, 2277, 2278, 2279, 2280, 2281, 2282, 2283, 2284, 2285, 2286, 2287, 2288, 2289, 2290, 2291, 2292, 2293, 2294, 2295, 2296, 2297, 2298, 2299, 2300, 2301, 2302, 2303, 2304, 2305, 2306, 2307, 2308, 2309, 2310, 2311, 2312, 2313, 2314, 2315, 2316, 2317, 2318, 2319, 2320, 2321, 2322, 2323, 2324, 2325, 2326, 2327, 2328, 2329, 2330, 2331, 2332, 2333, 2334, 2335, 2336, 2337, 2338, 2339, 2340, 2341, 2342, 2343, 2344, 2345, 2346, 2347, 2348, 2349, 2350, 2351, 2352, 2353, 2354, 2355, 2356, 2357, 2358, 2359, 2360, 2361, 2362, 2363, 2364, 2365, 2366, 2367, 2368, 2369, 2370, 2371, 2372, 2373, 2374, 2375, 2376, 2377, 2378, 2379, 2380, 2381, 2382, 2383, 2384, 2385, 2386, 2387, 2388, 2389, 2390, 2391, 2392, 2393, 2394, 2395, 2396, 2397, 2398, 2399, 2400, 2401, 2402, 2403, 2404, 2405, 2406, 2407, 2408, 2409, 2410, 2411, 2412, 2413, 2414, 2415, 2416, 2417, 2418, 2419, 2420, 2421, 2422, 2423, 2424, 2425, 2426, 2427, 2428, 2429, 2430, 2431, 2432, 2433, 2434, 2435, 2436, 2437, 2438, 2439, 2440, 2441, 2442, 2443, 2444, 2445, 2446, 2447, 2448, 2449, 2450, 2451, 2452, 2453, 2454, 2455, 2456, 2457, 2458, 2459, 2460, 2461, 2462, 2463, 2464, 2465, 2466, 2467, 2468, 2469, 2470, 2471, 2472, 2473, 2474, 2475, 2476, 2477, 2478, 2479, 2480, 2481, 2482, 2483, 2484, 2485, 2486, 2487, 2488, 2489, 2490, 2491, 2492, 2493, 2494, 2495, 2496, 2497, 2498, 2499, 2500, 2501, 2502, 2503, 2504, 2505, 2506, 2507, 2508, 2509, 2510, 2511, 2512, 2513, 2514, 2515, 2516, 2517, 2518, 2519, 2520, 2521, 2522, 2523, 2524, 2525, 2526, 2527, 2528, 2529, 2530, 2531, 2532, 2533, 2534, 2535, 2536, 2537, 2538, 2539, 2540, 2541, 2542, 2543, 2544, 2545, 2546, 2547, 2548, 2549, 2550, 2551, 2552, 2553, 2554, 2555, 2556, 2557, 2558, 2559, 2560, 2561, 2562, 2563, 2564, 2565, 2566, 2567, 2568, 2569, 2570, 2571, 2572, 2573, 2574, 2575, 2576, 2577, 2578, 2579, 2580, 2581, 2582, 2583, 2584, 2585, 2586, 2587, 2588, 2589, 2590, 2591, 2592, 2593, 2594, 2595, 2596, 2597, 2598, 2599, 2600, 2601, 2602, 2603, 2604, 2605, 2606, 2607, 2608, 2609, 2610, 2611, 2612, 2613, 2614, 2615, 2616, 2617, 2618, 2619, 2620, 2621, 2622, 2623, 2624, 2625, 2626, 2627, 2628, 2629, 2630, 2631, 2632, 2633, 2634, 2635, 2636, 2637, 2638, 2639, 2640, 2641, 2642, 2643, 2644, 2645, 2646, 2647, 2648, 2649, 2650, 2651, 2652, 2653, 2654, 2655, 2656, 2657, 2658, 2659, 2660, 2661, 2662, 2663, 2664, 2665, 2666, 2667, 2668, 2669, 2670, 2671, 2672, 2673, 26

doi:10.1017/S0022292410000507 Printed in the United Kingdom

Investigation of corrosion of metals by nonelectrolytes.
II. Action of cracked benzines on zinc. L. G. Gindin,
I. I. Torunov and R. S. Antarkumyan. *Bull. Acad. Sci.*
U.S.S.R., Chem. Div. Math. Sci. Ser. Chem. 1936, 25, 92
(in German 28 91); cf. *J. A. C. 30, 1936*. The assumption
that the aggressiveness of cracked benzines in causing
corrosion of metals is due to their autooxidation is proven
experimentally by subjecting weighed specimens of Zn
plates to the action of Gromeny and Bakin cracked ben-
zines for varying periods of time (up to 770 days). From
the exptl. results it is established that the intensity of cor-
rosion of Zn is a function of the acidity and amt. of tars
present in the benzines. Under certain conditions, a
"passive" film, probably composed of Zn and org. compds.,
forms on the Zn surface and protects it from further de-
compn. Eighteen references. John Livak

ASD 554 METALLURGICAL LITERATURE CLASSIFICATION

17

7A

7

Autoxidation of unsaturated hydrocarbons. P. Panyutin, L. Hingda and O. Vasil'eva. *Compt. rend. acad. sci. R. S. S. (N. S.)*, 2, 183-4 (1936) (in German).—To 2.5 ml. of the substance to be tested, e. g., benzene, add exactly 20 ml. of 4% KI in HCl and 0.5 ml. of pure, concd. H_2SO_4 . Allow the mixt. to stand 4 hrs. in the dark in a stoppered bottle. At the same time start a blank expt. with the same quantities of reagents and 5 ml. of distd. benzene which is known to contain no unsatd. compds. After the specified time has elapsed, titrate the I_2 in the blank test with $Na_2S_2O_3$. In the main expt. titrate the excess KI after oxidation with ferric alum soln. To accomplish this, ext. the soln. in the main test with two 50-ml. portions of water. Dil. the aq. ext. to exactly 250 ml. and take a 50-ml. aliquot. Transfer this to a 200-ml. round-bottomed flask carrying a glass stopper which is fitted with a glass delivery tube. Add 5 ml. of 25% H_2SO_4 , 2 g. of ferric alum and 2-3 pieces of calcite. Slowly heat the contents of the flask and pass the escaping gas into 100 ml. of 10% KI soln. which is kept cold with ice. Finally titrate the I_2 in the receiver with $Na_2S_2O_3$. In exactly the same way, treat 25 ml. of the KI soln. with ferric alum and det. the original I content. The peroxide no., expressed in g. I which would be used up by 100 g. of the substance analyzed, can be obtained by the formula, peroxide no. = $[a - b(b - c) - e]T/100 \cdot n \cdot d$, where a = ml. $Na_2S_2O_3$ required for titrating the I_2 originally present in the KI soln., b = ml. $Na_2S_2O_3$ required in titrating the distd. I_2 , c = ml. $Na_2S_2O_3$ required in the blank, T = titer of the $Na_2S_2O_3$ in terms of I , n = ml. of sample taken and d , its d. If it is desired to express the peroxide no. in terms of gram-equiv. of active O, as is usual, then the titer of the soln. should be in terms of O. W. T. H.

ASAC-51.6 METALLURGICAL LITERATURE

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Behaviour towards metals of solutions of sulphur and a range of organic sulphur compounds in saturated hydrocarbons. L. G. GUREVA, I. I. YANUS'YEV, and V. A. KARAKOVA (Compt. rend. Acad. Sci. U.R.S.S., 1959, 3, 219-223; cf. B., 1959, 694).—The role of S compounds in the corrosion of metals by fuel oils is discussed. Solutions of S in C_4H_{10} (free from S compounds) had no action on steel and Pb. during 16 months at room temp., but formed CuS on Cu . R. C. M.

R. C. M.

A B M - S L A METALLURGICAL LITERATURE CLASSIFICATION

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SECRET

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*Corrosion of Metals by Light Hydrocarbon Fuels. I. G. Gindin and
B. R. Ambarzumian (*Tekhnika Vozdush. Flota (Tech. Air Fleet)*, 1937,
(4), 88-92). [In Russian.] Aviation petrols from Gruzny and Baku
petroleum have no action on aluminum, Duralumin, ZAGI-11 alloy, American
alloy, magnesium, Elektron, zinc, copper, brass, or steel at 15-20°C, unless
water is present as a separate layer, in which case considerable corrosion occurs,
especially at the petrol-water interface. Since petrols obtained by the crack-
ing process readily oxidize on exposure to the air, with the formation of tarry
matter and organic acids, such petrols attack all the above metals strongly.
N A

GENERAL INFORMATION

1. TITLE: CORROSION OF METALS BY LIGHT HYDROCARBON FUELS

2. AUTHOR: GINDIN, I. G.; AMBARZUMIAN, B. R.

3. SOURCE: *Tekhnika Vozdush. Flota*, 1937, (4), 88-92.

4. SUBJECT: CORROSION; METALS; FUELS; ALUMINUM; DURALUMIN; ZAGI-11; MAGNESIUM; ELEKTRON; ZINC; COPPER; BRASS; STEEL; TEMPERATURE; 15-20°C; WATER; OXIDATION; TARRY MATTER; ORGANIC ACIDS.

5. SUMMARY: Aviation petrols from Gruzny and Baku have no action on various metals at 15-20°C unless water is present as a separate layer, in which case corrosion occurs. Cracked petrols oxidize on exposure to air, forming tarry matter and organic acids that attack the metals.

6. REFERENCES: None.

7. DISTRIBUTION: Limited.

8. AVAILABILITY: Restricted.

9. SECURITY CLASSIFICATION: CONFIDENTIAL.

10. REPORT NUMBER: 1.

11. CONTRACT NUMBER: None.

12. PROJECT NUMBER: None.

13. PROGRAM NUMBER: None.

14. TASK NUMBER: None.

15. SUBTASK NUMBER: None.

16. PERFORMING ORGANIZATION: None.

17. PERFORMING ORGANIZATION REPORT NUMBER: None.

18. DISTRIBUTION STATEMENT: CONFIDENTIAL.

19. DISTRIBUTION STATEMENT: CONFIDENTIAL.

20. DISTRIBUTION STATEMENT: CONFIDENTIAL.

BC

Linear corrosion of metals. I. Selective corrosion of metals on three-phase boundaries. L. O. GUMST, D. R. MILLER, and F. M. SCHNEIDER (J. Phys. Chem. Res., 1937, 5, 91-103).—The corrosion of Cu by 48.3% H_2SO_4 of 30% H_2SO_4 and of Mg by HCl and NaOH occurs strongly on the three-phase boundary metal-paraffin-corrosive liquid, causing the formation of deep pits around a paraffin spot on the metal surface. This linear corrosion is sometimes a pitting process. The linear corrosion on the phase boundary does not depend on surface activity of the corroding liquid and is not affected by addition of surface-active substances. E. R.

Corrosion of metals by nonelectrolytes. Influence of light hydrocarbon fuel on metals and alloys. IV. Action of cracked gasoline on steels. L. G. Kuzmina and R. S. Anisatsumyan. *J. Phys. Chem. U.S.S.R.* 9, 230-231 (1977), cf. C. A. 31, 4252. Corrosion of steel is strongly controlled by cracked gasoline in 400,000 days at room temp. Corrosion is coupled with autooxidation of the gasoline. Stainless steel (Austenitic) is not attacked in 400 days. V. Action of cracked gasoline on copper and brass. *Ibid.* 222-231. Cu is strongly corroded in cracked gasoline in 400 days at room temp.; the loss in wt. are up to 2.5 g. per 100 g. Corrosion is due to autooxidation of the gasoline. No autooxidation of copper occurs in presence of a 2 ppm. antioxidant. Brass is strongly corroded by gasoline from Baku, but only slightly by that from Grozny. The corrosion of brass is associated with a dezincification. R. C. A.

ASH 55A METALLURGICAL LITERATURE CLASSIFICATION

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***Metal Corrosion by Non-Electrolytes. Influence of Light Hydrocarbon
Fuels on Metals and Alloys. V.---Action of Cracked Petrols on Copper and
Brass. I. (I. Gindly) and R. M. Ambarzumian (Zaur. Fizik. Khim. (J.
Phys. Chem.), 1937, 9, (2), 228-230). (In Russian.) Copper is strongly
attacked by oxidized cracked petrol, and the action is controlled by the rate
of autoxidation of the petrol and by the corrosion products. The actual loss
in weight of the metal depends on the changes which occur in the composition
of the oil; the results obtained with petrol derived from Baku oil differ
from those obtained with petrol from Grozny oil. Both petrols attack β and
 $\alpha + \beta$ brass, producing dezincification.---N. A.**

ASB SLA METALLURGICAL LITERATURE CLASSIFICATION

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A-1

Linear corrosion of metals. Selective corrosion of iron by the system water-sulphuric acid-propyl alcohol on three-phase boundaries. L. GINDEL and F. SOHREMAKER (Compt. rend. Acad. Sci. U.R.S.S., 1937, 26, 400-412; of A., 1937, 1, 319).—The corrosion of Fe, partly covered with paraffin, in $H_2O-H_2SO_4-PrOH$ mixtures has been investigated. Concn. ranges which yield linear attack at the air-liquid and liquid-paraffin interfaces, periodic formation of films of corrosion product, and resinification of the $PrOH$ are distinguished. J. W. S.

130-354 METALLURGICAL LITERATURE CLASSIFICATION

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Relation to metals of sulphur solutions and of a series of organic sulphur compounds in saturated hydrocarbons. Relations to iron of ethyl and butyl mercaptan solutions in cyclohexane. L. Q. GINSBURG, L. I. TOROSJAN, and V. A. KAZAKOVA (Compt. rend. Acad. Sci. U.R.S.S., 1937, 16, 413-418).—Fe is unaffected by solutions of EtSH and BuSH in cyclohexane. It is confirmed that the lamp method is satisfactory for determination of S in oils.

J. W. S.

454 514 METALLURGICAL LITERATURE CLASSIFICATION

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Research on autoxidation of unsaturated hydrocarbons.
1. Determination of peroxides in the presence of unsaturated compounds. P. S. Panyutin and L. G. Gudin. *Bull. acad. sci. U. R. S. S., Classe sci. math. nat., Ser. chim.* 1938, 841-83 (in English, K33-4). — The method depends upon treatment of the sample with 4% KI in alc. in the presence of H_2SO_4 . The excess KI is extd. with water, oxidized by ferric alum soln. The liberated I_2 is absorbed in KI soln. and titrated with $Na_2S_2O_3$. The method is suitable for detg. peroxide in gasoline. Seventeen references. J. G. Tolpin

AVH SLA METALLURGICAL LITERATURE CLASSIFICATION

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Oxidation of alkyl anthraquinones and their derivatives. I. Oxidation with chromic anhydride of β -methylanthraquinone to anthraquinone- β -carboxylic acid. M. A. Il'in, N. F. Chibrikova and V. A. Kuzakova. *Compt. rend. acad. sci. U. R. S. S. S. 20, 555 (1958)* (in English). A method of oxidation of β -methylanthraquinone (I), giving 96% of anthraquinone- β -carboxylic acid (II), has been developed by the following procedure. To 1 g I in 50 ml warm glacial AcOH was added gradually 3 g finely ground anhyd. CrO₃ with vigorous stirring; the mixt. was warmed to 70° and held there for 8 hrs.; the contents were cooled, dil. with 100 ml H₂O, and the ppt. filtered, washed with H₂O, boiled with dil. NH₃ soln. till the filtrate no longer gave a ppt. upon acidification; the soln. of the NH₃ salt of II was filtered and the filtrate acidified with HCl, giving II, m. 201-2°. The highest yields were obtained with anhyd. AcOH and CrO₃. II. Oxidation of β -methylanthraquinone with chromic anhydride to anthraquinone- β -carboxylic acid as influenced by water. *Ibid.* 556-60. Using the above oxidation conditions, the inhibiting action of H₂O was detd. The yield of anthraquinone- β -carboxylic acid was decreased with increase in the amt. of H₂O added. The results are tabulated. I. F. I.

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Investigations of the corrosion of metals by nonelec-
trolytes. The action of light hydrocarbon fuel on metals
and alloys. VI. The action of cracked gasoline on lead.
I. G. Gladin. *Compt. rend. acad. sci. U. R. S. S. 20*,
561-4 (1958) (in English); *J. C. A. 33*, 2004. When
autooxidation occurs in Baku and Grozny cracked gasolines
contg. metallic Pb, the Pb is strongly corroded. With
the Baku material, 13.2 g. of Pb is attacked after 710
days in 100 cc. of the gasoline. Analysis shows that
about 60% of the corrosion product is $PbCO_3$. It is
suggested that org. acids formed on autooxidation first
attack the Pb, then CO_2 displaces part of the org. acid in
the Pb salt.
George Avery

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Kinetics of the polymerization of 3-chloro-1,3-butadiene catalyzed by benzoyl peroxide in dibutyl phthalate solutions. S. S. Medvedev, L. Olgin and M. Lazareva. *J. Phys. Chem.* (U. S. S. R.) 13, 1280-1402 (1970).--
The kinetics of the polymerization of chloroprene (I) and the distribution of I in the gas and liquid phases were detd.

2

by a manometric method. The soly. of I in dibutyl phthalate is given by $P/C^* = K$ with $n = 0.730$, $K = 2.15$ at 30° ; $n = 0.822$, $K = 3.03$ at 60° . The polymerization process is heterogeneous; the rate increases with increasing concn. of I and benzoyl peroxide (II) only up to a certain max. and then remains const. This max. is greater the greater the surface available, varying from 2 to 8% II. With 4% II, the energy of activation between 30 and 60° is 12.5 Cal. On the basis of an analysis of the kinetic data, it is concluded that the initial active centers form as the result of reaction between I and ionized II radicals adsorbed on the walls. These reaction nuclei then leave the wall and the polymerization process takes place in the soln. vol. Deactivation may occur either by reaction with un-ionized II or by collision with adsorbed mols. of I.

F. H. Rathmann

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Corrosion of Metals by Non-Aqueous Solutions. The Action of Ethyl Alcohol on Metals. L. Q. Gindin, R. S. Ambarzumian and R. P. Melchikov. (Comptes Rendus (Doklady) de l'Académie des Sciences de l'U.R.S.S., 1940, vol. 20, Oct. 10, pp. 44-47). This is the introductory paper to a projected series on the corrosion of metals in non-aqueous electrolytes, mainly alcohols and alcoholic solutions. The authors review the literature on the effect of ethyl alcohol on metals, and they describe the procedure they adopted for the purification of the ethyl alcohol used for their investigation. In the series of experiments described in the present paper, the tests were carried out in sealed glass tubes in an apparatus which is illustrated, and tables are given of the results obtained after keeping samples of magnesium, aluminium, zinc and steel (carbon 0.28%, manganese 0.51% and silicon 0.22%) for 210 days under absolute alcohol and for 180 days under 99.7% alcohol. Only magnesium proved to be slightly corroded by ethyl alcohol under the experimental conditions described, whereas the three other materials examined were not affected at all.

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Corrosion of Metals by Non-Aqueous Solutions. R. S. Ambarzumian, I. G. Gladin and E. P. Balchikova. (Comptes Rendus (Doklady) de l'Académie des Sciences de l'U.R.S.S., 1940, vol. 29, Oct. 20, pp. 91-94). The authors studied the influence of carbon dioxide on the action of ethyl alcohol on magnesium, aluminium and steel. They used alcohol saturated with carbon dioxide, and the experimental procedure was as described in the first paper of the series (see preceding abstract). They found that in the presence of carbon dioxide, steel and aluminium are also not corroded by ethyl alcohol, whereas the corrosion of magnesium is considerably enhanced.

METALLURGICAL LITERATURE CLASSIFICATION

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STONY BROOK

Corrosion of metals by nonaqueous solutions I. G. Gindin, R. S. Ambaturmjan and E. P. Belchikova (*Cheml. Zh. i. Prikl. Khim.*, 1960, 24, 204-20 (in Russian)). The inactivity of EtOH on metals was examined with respect to the possible presence of "antimobilizers" such as aldehydes or fuel oils. Two metals Mg and Fe-tron metal (1) were tested as described in previous experiments for a period of 180 days at 20 mm Hg, free from aldehydes and fuel oil, and in the same alk. to which was added separately, 0.1% of formaldehyde, acetaldehyde, paraldehyde and benzaldehyde. The addition of formaldehyde and acetaldehyde produced no inhibition. Paraldehyde inhibited completely the corrosion of Mg and greatly decreased that of Fe. Benzaldehyde decreased the corrosion of Fe by a factor of 3. Expt. showed, however, that in alk. with CO₂, none of the above aldehydes was effective in reducing the corrosion. I. K.

AS 11.1 METALLURGICAL LITERATURE CLASSIFICATION

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The mechanism of the simultaneous polymerization of butadiene with vinyl cyanide and 1-methylvinyl cyanide under the action of benzoyl peroxide. L. Gindin, A. Abkin, and S. Medvedev (Karpov Inst. Phys. Chem., Moscow). *J. Phys. Chem. (U.S.S.R.)* 21, 1299-87 (1947) (in Russian).—Mists of butadiene (I) (x wt. %) with CH_2CHCN (II) (100 - x %) or $\text{CH}_2\text{CH}(\text{CN})_2$ (III) (100 - x %) and $(\text{BuO})_2$ (y %) were prep. in N_2 heated 1 hrs., and distd. at room temp. in a high vacuum 20 hrs. The distn. residue (= polymer) was analyzed for N (i.e. nitrile) and active O (i.e. BuO). For the detn. of active O the polymer must be dissolved in CHCl_3 , not in acetone. The rate ν of formation of polymer decreases when x increases; e.g. at 60° for the system I + II (y being 0.6%) increases; e.g. at 60° for the system I + II (y being 0.6%) the initial rate is 0.26% per hr. at x = 90% and 8.8% per hr. at x = 20%. During one expt. ν is almost const. at small x and increases with time at large x. The ν increases with temp.; e.g. 42° polymer is attained at 50° within 63 hrs. and at 70° within 11 hrs. The ν is proportional to \sqrt{y} between y = 0.3 and y = 10 wt. %. These results are discussed from the viewpoint of Abkin and Medvedev, *C.A.* 34, 77(9). The polymerization ceases when one of the components is used up. The highest yield of polymer

(over 80%) is observed at x = 50% for the I + II and near x = 70% for the I + III system. The compn. of the polymer depends little on the time of polymerization and temp., but varies according to x. In the I + II system, the polymer contains more I than the original mixt. at x < 53% and less than the original mixt. at x > 53%. In the I + III system, the "azeotropic" mixt. has x = 60%. The concn. of $(\text{BuO})_2$ in the polymer decreases when t increases. However, polymerization continues also after this concn. becomes zero. Monomer, distd. from the polymer and again mixed with it, polymerizes at the same ν as if no distn. occurred, but soln. and reprecip. of polymer remove its catalytic activity. The compn. of a copolymer depends on the constn. α and β expressing the relative rates of reaction of 2 free radicals with the 2 components of the monomeric mixt. A simple method for computing α and β from exptl. data is shown. From the values for α and β the distribution of monomer groups within the copolymer can be calcd. (cf. *C.A.* 42, 8046). In the copolymer I + II, 67% II is present as one nitrile group between 2 butadiene groups; and in I + III 80% III is in this alternate pattern. The cessation of polymerization when 1 of the components is used up shows that both components are needed for the branching of the reaction chain.

J. J. Bikerman

ASH 3.4 METALLURGICAL LITERATURE CLASSIFICATION

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USSR/Metals

Copper

Corrosion

Dec 48

"Anthraquinone Protection of Copper From Corrosion
by Sulfur Solutions," L. G. Gindin, R. Kh. Sil's,
All-Union Inst Avn Materials, 4 pp

Dokl Ak Nauk SSSR" Vol LXIII, No 6

Shows that anthraquinone lengthens period of "in-
hibition," which precedes beginning of corrosion,
by 500,000 times. Table shows effect of anthraquinone
on corrosion of copper by sulfur solutions. Decides
that anthraquinone cannot properly be called an in-
hibitor, or its effect be called inhibition since it
35/49767

USSR/Metals (Contd)

Dec 48

does not slow the reaction but rather moves back its
beginning, or "immunizes" the metal. Submitted by
Leonid A. B. Franklin, 3 Nov 48.

35/49767

Polymerization of allyl acrylate. 1. Determination of the structure and molecular weight of the soluble forms of polyallyl acrylate. L. Gindin, S. Medvedev, and E. Flesher. *Zhur. Obshchei Khim.* (J. Gen. Chem.) 19, 1081 (1949). - Polymerization of allyl acrylate, bp. 119-121.5°, n_D^{20} 1.4330, d_4^{20} 0.888 (7), in 2.5 and 5.7% solns. in CCl_4 with 1% BaO_2 catalyst at 60° gives low mol. products, sol. in org. solvents, with the main chain linkage formed substantially from the "acrylic" double bond. The process, followed dilatometrically to 80% polymerization, gave 35.0% total unsatn. of the product, which was almost identical with the "allyl" unsatn. by the bromide-bromate method in CCl_4 , $AcOH$; the total unsatn. was detd. by the bromide-bromate method in the presence of $HgSO_4$; the procedures were successfully tested on the monomer. G. M. Kowaloff.